





# **Enhancing Microgrid Flexibility and Dynamic Performance with Inverter-based Resources (IBRs)**

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# **Contents**

- **Introduction**
- **Inverter P-Q Control with Trajectory Tracking Capability Based on Physics-informed Reinforcement Learning**
- **Decentralized and Coordinated V-f Control Considering DER Inadequacy and Demand Control**
- **Virtual Inertia Scheduling for low inertia IBR-based Power Grids**
- **Take Aways**



# **Microgrid definition**



**A typical microgrid**

### **Definition**

❑ An integrated energy system composed of multiple **distributed energy resources (DERs), energy storage systems, and local loads**, which can operate in either grid-connected mode or islanded mode.

### **Characteristic**

- ❑ Small system size
- ❑ High penetration of **inverter-based resources (IBRs)**
- ❑ Low system inertia
- ❑ High R/X ratio of the feeders
- ❑ Strong voltage and frequency (V-f) coupling

# **Challenges and Opportunities**

### ➢ **Challenges**

- Higher uncertainty
- Elements that are difficult to model
	- Customer behavior
	- Extreme weather
- Model and parameter accessibility/Privacy
- Faster dynamics of IBRs
- Requirement for improved resilience

### ➢ **Opportunities**

- Renewable Energy
- Flexibility and Controllability of IBRs
	- o Address uncertainty
	- Provide grid dynamic support
	- Supply critical load
- Cutting-edge techniques
	- o Deep learning
	- o Reinforcement learning

*Challenges and opportunities coexist in microgrids, and the key point is how we effectively manage the challenges and utilizing the existing resources.*



**High-level research map of microgrid control** 



RENT

**presentation focus**

**Marks the** 

B. She, F. Li, H. Cui, J. Zhang, and R. Bo, "Fusion of Microgrid Control with Model-Free Reinforcement Learning: Review and Vision," *IEEE Transactions on Smart Grid*, vol. 14, no. 4, pp. 3232-3245, July 2023.



# **Presentation Outline**





### **Contents**

- **Introduction**
- **Inverter P-Q Control with Trajectory Tracking Capability Based on Physics-informed Reinforcement Learning**
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# **Objective: Guaranteed Trajectory**

### ➢ **Objective**

Assume a step input, the PQ output of **grid-following** IBRs can be controlled smoothly and accurately

 $y(t) = 1 - e^{-t/\tau}$ 

Where  $\tau$  is response time constant that can be freely assigned.

### ➢ **Benefits**

Improve the **controllability** and **flexibility** of IBRs

- $\circ$  Intentional power injection  $\rightarrow$  large time constant
- $\circ$  Emergency support  $\rightarrow$  small time constant



*Key Idea:* the actual response following the desired trajectory



H. Li, F. Li, Y. Xu, D. T. Rizy, and J. D. Kueck, "Adaptive Voltage Control with Distributed Energy Resources: Algorithm, Theoretical Analysis, Simulation and Field Test Verification," *IEEE Transactions on Power Systems*, vol. 25, no. 3, pp. 1638-1647, August 2010.

# **Methodology: Adaptive gains**

### ➢ **Methodology**

( ) **Methor**<br>
( **Internal Contains transferred transferred transferred transferred transferred transferred transferred to the controller in**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and Meth**<br>PI controller with<br>o ensure the acturing the desired to  $k_p = f(t)$ <br>adaptive controller **Meth**<br>
Introller with<br>
sure the acturate desired to<br>  $f(t)$ <br>
otive controller<br> **g** (*t*)<br>
otive controller Use **adaptive** PI controller with timevarying gains to ensure the actual response following the desired trajectory

$$
\begin{cases}\nk_p = f(t) \\
k_i = g(t)\n\end{cases}
$$

- o Implement the adaptive controller in the outer **PQ regulation loop**, because it has lower bandwidth and its output determines the inverter PQ response
- o Do model-based analysis to **inform** the reinforcement learning based implementation



**Diagram of the Proposed Adaptive Inverter PQ Controller**

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### **Model-based Analysis**





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 $\overline{\mathcal{L}}$ 

B. She, F. Li, H. Cui, H. Shuai, O. Oboreh-Snapps, R. Bo, N. Praisuwanna, J. Wang, L. M. Tolbert, "Inverter PQ Control with Trajectory Tracking Capability for Microgrids Based on Physics-informed Reinforcement Learning," *IEEE Transactions on Smart Grid*, In-Press, 2023.

# **Data-driven Implementation: DRL**



### **Reinforcement learning :**

❑ RL is a basic machine paradigm formulated as a Markov Decision Processes.

### **Deep reinforcement learning:**

❑ Use **deep neural network** to map: State, action  $\rightarrow$  value (Q-value); State  $\rightarrow$  action

### **Training Target:**

❑ *a well-trained RL agent chooses optimal actions for maximum accumulated reward (best performance)*



# **Physics-informed DRL and HIL Test**



❑ Model-based analysis reduce learning space from **function space** to **real space**



**Diagram of Physics-informed Reinforcement Learning (RL) in the Numerical Simulator and Power HIL demonstration in HTB**



# **Test Microgrid and Training Results**



**Diagram of modified Banshee microgrid**





**Reward curve with and without model-based analysis**

# **Validation in MATLAB-Simulink**



**▷ Scenario 1-2**: Scheduling  $P_{ref}$  and  $Q_{ref}$  change ▶ Scenario 3: Grounded fault





# **Validation in CURENT HTB**



### **Scheduling reference change Generation reduction & recovery**

- ❑ Inverters can be freely assigned **any time constant** and respond either slow or fast to changing commands.
- ❑ The proposed control algorithm is valid under the **power hardware-in-the-loop demonstration**.



# **Summary**

❑ There exists a time-varying-gain adaptive PI controller that can track a **predefined exponential trajectory** for microgrid inverter-based PQ control.

- ❑ The proposed controller outperforms the conventional fixed-gain and adaptive PI controllers. **Without manual re-tuning**, it can accurately track the predefined trajectory with any assigned time constant.
- ❑ The **model-based analysis** provides guidelines for deep RL training, which relieves the training pressure and saves training time. In turn, the implementation of **physics-informed deep RL**  solves the problem of unavailability and uncertainty in the model-based method.



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# **Background and Motivation**

**over-load**

**T ransition zone**

**Inadequate**

### ➢ **Background**

An islanded microgrid forms a self-sufficient system with **gridforming IBRs** supplied by distributed energy resources (DERs).

DER inadequacy under various load level ➢ **Challenges**

**D E R C apacity:**

**L oad C ondition:**

Conflict between fluctuating DC side DERs capacity and automatic load sharing based on fixed droop gains.

**A dequate**

**light-load heavy-load**

- o **IBR saturation** caused by overloads
- o Large frequency and voltage **deviation**
- o Unexpected DC voltage dip and **IBR trip**





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# **Objective**

### ➢ **Objective**

- o Accurately control the **output of GFM inverters** when DER is insufficient;
- o **Improve load sharing** results based on real-time DER capacity;
- o **Coordinate** voltage and frequency (V-f) regulation under the condition of constrained DER capacity;

### ➢ **Benefits**

- o Improve the **controllability** and **stability** of IBRs
- o Make the best use of limited DER capacity
- o Reduce V-f deviation
- o Reduce involuntary load shedding



Constrained operation of IBRs

# **Methodology (1)**

### ➢ **Key idea**

- o Generate **supplementary signal**  based on real-time DER capacity and feed it to **primary regulator**
- o Consider the impact of load sensitivity to voltage and frequency



Diagram of a droop-controlled GFM inverter supplying V-f dependent load



# **Methodology (2)**

### ➢ **Proposed Control framework**



Diagram of the proposed decentralized and coordinated control framework

### Input  $\left\{\begin{array}{c} \downarrow s, \\ \downarrow \downarrow s, \\ \downarrow \downarrow s \end{array}\right\}$   $\Box$  Power regulator and V-f regulator generate **supplementary signals** for the primary regulator

- **EX** DER capacity, which help limit the output of grid-❑ **Power regulator** generates control signals based on the error between inverter output and forming inverters
- $V^{\text{IV}}_{\text{A}}$   $V^{\text{IV}}_{\text{M}}$  *v*<sub>m</sub>  $V^{\text{IV}}_{\text{M}}$  voltage and frequency deviations, which ❑ **V-f regulator** generates control signals based on reallocates limited generation for acceptable V-f deviations

# **Proposed Approach (1)**

### ➢ **IBR integrated power flow**

A general islanded microgrid formed by *N* **inverters**, each inverter is connected to an independent bus with a local V-f dependent load

**Proposed Approach (1)**  
\n**IBR integrated power flow**  
\nA general islanded microgrid formed by **N** inverters, each inverter is connected to an independent bus  
\nwith a local V-f dependent load  
\n
$$
\begin{cases}\nf = f_{0,i} + k_{dj}(P_{im,j} - P_{im0,i}) & \forall i = 1, 2, L, N \\
V_i = V_{0,i} + k_{dv}(Q_{im,j} - Q_{im0,i}) & \forall i = 1, 2, L, N\n\end{cases}
$$
\n*Proof equation*  
\n
$$
\begin{cases}\nP_{i,i} = P_{0,i}(p_i V_i^2 + p_2 V_i + p_3) \left[1 + K_{pj}(f - f_0)\right] & \forall i = 1, 2, L, N \\
Q_{i,i} = Q_{i0,i}(q_i V_i^2 + q_2 V_i + q_3) \left[1 + K_{pj}(f - f_0)\right] & \forall i = 1, 2, L, N\n\end{cases}
$$
\n*2N*  
\n
$$
\begin{cases}\nP_i = P_{im,j} + P_{i,ii} = G_{ij} V_i^2 - G_{ij} \sum_{i \neq j} V_i V_j \cos \theta_{ij} - B_{ij} \sum_{i \neq j} V_i V_j \cos \theta_{ij} \\
Q_i = Q_{im,i} + Q_{i,i} = G_{ij} V_i^2 - G_{ij} \sum_{i \neq j} V_i V_j \cos \theta_{ij} - B_{ij} \sum_{i \neq j} V_i V_j \cos \theta_{ij}\n\end{cases}
$$
\n**6N decision variables:**  
\n**6N decision variables:**  
\n1 **do** A active inverter output, and N reactive inverter output. *N* active load, N active interter output, and N reactive inverter output.

### **6***N* **decision variables:**

1 global frequency, *N* voltage, *N*-1 power angle, *N* active inverter output, *N* active load, *N* active inverter output, and *N* reactive inverter output.

# **Proposed Approach (2)**

### ➢ **IBR integrated power flow considering the proposed framework**

- o Primary regulator become invalid due to DER inadequacy
- o *2N* Droop equations are changed to *N* capacity constraints



### ➢ **New equilibrium**

- $\circ$  Given  $(P_{inv,i}, Q_{inv,i})$  on the capacity circle, there are **4***N* state variables and **4***N* equations left.
- o Then for each (*Pinv,i*', *Qinv,i*'), the corresponding new equilibrium V-f is solvable.

Show the existence of new **equilibrium** when integrating the proposed control framework

![](_page_23_Picture_9.jpeg)

B. She, F. Li, H. Cui, J. Wang, L. Min, O. Oboreh-Snapps, R. Bo, "Decentralized and Coordinated V-f Control for Islanded Microgrids Considering DER Inadequacy and Demand Control," *IEEE Transactions on Energy Conversion*, vol. 38, no. 3, pp. 1868-1880, Sept. 2023.

# **Case Study in An Ideal System**

### ➢ **IBR-based 3-bus system**

![](_page_24_Figure_2.jpeg)

- $\circ$  Assume the total load is close to but small than the total DER capacity
- o An intentional load increase at the initial operating point (*P*<sup>0</sup> , *Q*<sup>0</sup> ) and the total load **exceed** the DER capacity.
- o Predict the **new equilibrium**

![](_page_24_Figure_6.jpeg)

V-f deviation under bounded generation constraints

![](_page_24_Picture_8.jpeg)

# **Case study in a Real Microgrid (1)**

### ➢ **Modified Banshee Microgrid**

![](_page_25_Figure_2.jpeg)

**Single-line diagram of modified Banshee microgrid** RENT

### **Table. 1 Control parameters of grid-forming inverters**

![](_page_25_Picture_464.jpeg)

# **Case study in a Real Microgrid (3)**

![](_page_26_Figure_1.jpeg)

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**V-f response: increase Q, decrease P**

# **Case study in a Real Microgrid (4)**

![](_page_27_Figure_1.jpeg)

**Scenario 2: P-Q regulator + V-f regulator**

**Dynamic inverter output**

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![](_page_27_Figure_3.jpeg)

**V-f response: increase P, decrease Q**

# **Summary**

❑ **DER inadequacy** poses challenges to the operation of grid-forming inverters in islanded microgrids.

❑ **Power regulator** limits the output of grid-forming inverters by generating supplementary control signals based on the error between inverter output and DER capacity.

❑ **V-f regulator** generates control signals based on voltage and frequency deviations, which reallocates limited generation for acceptable V-f deviations.

![](_page_28_Picture_4.jpeg)

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![](_page_29_Picture_6.jpeg)

# **Motivation and Objective**

### ➢ **Background**

The penetration of **IBRs** decrease the **inertia** of microgrids. Existing research address low inertia problems by

- o **Device-level Control**: Design new control algorithm to improve the inertia support capability of IBRs
- o **Grid-level Dispatch**: integrate dynamic frequency constraints into the economic operation framework

**Decoupled** in the conventional synchronous generator (SG) dominant system because

- o Distinct time scales
- o Physical inertia of SGs is fixed

### **IBRs make a difference !**

### ➢ **Objective**

Develop a **unified inertia management** 

**framework** that combines the device-level control and grid-level economic operation and leverages the inertia support capability of grid component.

![](_page_30_Figure_12.jpeg)

**Diagram of virtual inertia scheduling for future low inertia microgrids**

# **Virtual Inertia Scheduling (VIS)**

### ➢ **Concept of VIS**

- o **VIS**: an inertia management framework that targets **security-constrained** and **economy-oriented** inertia scheduling and generation dispatch of microgrids with a large scale of IBRs.
- o **VIS** schedules the power setting points, as well as the **control modes** and **control parameters** of IBRs to provide secure and cost-effective inertia support.

VIS can be integrated into the existing economic operation framework, i.e., UC, RTED, and AGC.

B. She, F. Li, H. Cui, J. Wang, Q. Zhang, R. Bo, "Virtual Inertia Scheduling for Real-time Economic Dispatch of IBR-penetrated Power Systems," *IEEE Transactions on Sustainable Energy*, In-Press, 2023. ➢ **General Formulation of VIS**  $\prod_{i} \prod_{j} \prod_{j} C_{ge}$ <br>  $\min_{i} C_{ge}$ <br>  $\prod_{j} \prod_{j} M_{i}^{r}$ <br>  $\prod_{j} M_{i}^{r}$ **general Formulation of \<br>** *general Formulation of \***<br>** *min* $C_{gen}(P) + C_{aux}(P, M, I)$ **<br>
<b>Generation cost**<br>
1) Standard dispatch const<br>  $C_{off}(M, I)$ <br>  $M_i^{min, ibr} \leq M_i^{ibr} \leq M_i^{max, ibr}$ **Inertia support cost Generation cost**

\n- ✓ General Formulation of VIS **Inertia support cost**
\n- $$
\min_{P,M,D} C_{gen}(P) + C_{aux}(P, M, D)
$$
\n- **Generation cost**
\n- s.t. 1) Standard dispatch constraints
\n- $\left\{ M_i^{\min,ibr} \leq M_i^{ibr} \leq M_i^{\max,ibr}, \forall i \in \{1, \cdots, N_{ibr}\}$
\n- $2 \right\}$ \n $\left\{ D_i^{\min,ibr} \leq D_i^{ibr} \leq D_i^{\max,ibr}, \forall i \in \{1, \cdots, N_{ibr}\}$
\n- $3 \right\}$ \n $\left\{ -RoCof_{\lim} \leq f_0 \frac{\Delta P_{e,t}}{M_t} \leq RoCof_{\lim}, \forall t \in \{1, L, T\}$
\n- 4) Stability constraints\n  $\Delta$  Multiply dispatch or minutes dispatch\n  $\Delta$  Single stage or multiple stage\n  $\Delta$  Normal load change or given *contingency* set
\n

- 4) Stability constraints
- o *Hourly* dispatch or *minutes* dispatch
- o *Single* stage or *multiple* stage
- o *Normal* load change or given *contingency* set

### ➢ **VIS for Real-time Economic Dispatch (VIS-RTED)**

- o RTED: a multi-interval optimization problem with the objective of minimizing the total generation cost
- o Specified VIS-RTED
	- 1) One-hour dispatch with 12 intervals
	- 2) Quadratic generation cost
	- 3) Opportunity cost caused by inertia support

4) Additional decision variables of virtual inertia and damping

5) Additional dynamic constraints of frequency nadir and RoCof

### *Question*

*" How to quantify and then linearize* dynamic power of IBR ( $\Delta P_{peak}^{ibr}$  ) and frequency nadir ( $\Delta f_{nadir}$ )?" **objective: Minimize quadratic generation cost** 

**nonic Dispatch**  
\n
$$
\min_{P,M,D} \sum_{t \in T} \left[ \sum_{j=1}^{N_{sg}} (a_{i,t}^{sg} P_{i,t}^{sg} + b_{i,t}^{sg} P_{i,t}^{sg} + c_{i,t}^{sg} + b_{i,t}^{sg} P_{i,t}^{sg})
$$
\n
$$
+ \sum_{j=1}^{N_{br}} (a_{i,t}^{ibr} P_{i,t}^{ibr} + b_{i,t}^{ibr} P_{i,t}^{ibr} + c_{i,t}^{ibr} + b_{i,t}^{ibr} A P_{i,t}^{ibr})
$$
\n
$$
+ \sum_{j=1}^{N_{br}} (a_{i,t}^{ibr} P_{i,t}^{ibr} + b_{i,t}^{ibr} P_{i,t}^{ibr} + c_{i,t}^{ibr} + b_{i,t}^{ibr} A P_{i,t}^{ibr})
$$
\n
$$
\text{1. 1) Power balance + line limit constraints}
$$
\n
$$
\sum_{j} \begin{cases} P_{s,i,t}^{ibr} + P_{i,ru,t}^{ibr} + \frac{\Delta P_{i,pedk,t}^{ibr}}{\Delta P_{i,pedk,t}} \leq P_{i,t}^{\max, ibr} \ \forall t \in \{1, L, T\} \\ P_{s,i,t}^{ibr} - P_{i,rd,t}^{ibr} - \frac{\Delta P_{i,pedk,t}^{ibr}}{\Delta P_{i,pedk,t}} \geq P_{i,t}^{\min, ibr} \ \forall t \in \{1, L, T\} \end{cases}
$$
\n
$$
\text{3) } \begin{cases} M_{i}^{\min, ibr} \leq M_{i}^{\min} \leq M_{i}^{\max, ibr}, \forall i \in \{1, \dots, N_{ibr}\} \\ D_{i}^{\min, ibr} \leq D_{i}^{\max, ibr}, \forall i \in \{1, \dots, N_{ibr}\} \end{cases}
$$

s.t. 1) Power balance + line limit constraints

( )] 1 4 4 4 4 4 44 2 4 4 4 4 4 4 43 max, , , , , , , ,min, , , , , , , , 1, , 1, , *ibr ibr ibr ibr s i t i ru t i peak t i t ibr ibr ibr ibr s i t i rd t i peak t i t P P P P t T P P P P t T* + + − − L L min, max, min, max, , 1, , , 1, , *ibr ibr ibr i i i ibr ibr ibr ibr i i i ibr M M M i N D D D i N* , lim 0 lim min 0 , max , 1, , , 1, , *e t t nadir t P RoCof f RoCof t T M f f f f t T* − + L L 2) 3) 4)

![](_page_33_Figure_2.jpeg)

Uniform frequency dynamics model of IBR-penetrated grids

2  $2\sigma$ <sup>- $\zeta w_n t_m$ </sup>  $2$   $L^{\bullet}$   $V^{\bullet}$   $\rightarrow$  $\mathcal{P}_{\max}^{ibr} = \frac{\Delta T_e D_{ibr}}{MT_{sp}^2} \left[ -1 + \alpha \eta' e^{-\zeta w_n t_m} \right] \sin(\zeta)$  $\begin{aligned} &\frac{\Delta P_e}{MTw_n^2}\bigg[1-\sqrt{1-\boldsymbol{\zeta}^2}\boldsymbol{\eta}e^{-\boldsymbol{\zeta} w_nt_m}\bigg]\ &\frac{\Delta P_e D_{ibr}}{MTw_n^2}\bigg[-1+\boldsymbol{\alpha\eta}^\top e^{-\boldsymbol{\zeta} w_nt_m^\top }\sin(w_dt+\end{aligned}$  $-\zeta w_n t_m$  $\left[\Delta f_{nadir} = \frac{\Delta P_e}{MTw_n^2} \left[1 - \sqrt{1 - \zeta^2} \eta e^{-\zeta w_n t_m}\right]\right]$ <br>A pibr  $\Delta P_e D_{ibr} \left[1 + \exp\left(-\frac{\zeta w_n t_m}{2}\right) \sin(\omega t)\right]$  $\zeta_{w_n t_m}$  $\zeta w_n t_m$  cin(u) t **Dynamic index:**

➢ **Dynamic estimation** ➢ **Deep learning assisted linearization**

**omic Dispatch**  
\n
$$
\oint \Delta f_{nadir} = NN_1 (\Delta P_e, M, D, R, F, T)
$$
\n
$$
\Delta P_{max}^{ibr} = NN_2 (\Delta P_e, M, D, R, F, T)
$$
\n
$$
\begin{aligned}\n\text{hidden layer of neural} &\begin{cases}\n\hat{z}_m = W_m z_{m-1} + b_m \\
\text{with ReLU} \\
\text{ation function:}\n\end{cases} \\
\begin{cases}\n\hat{z}_m = W_m z_{m-1} + b_m \\
\hat{z}_m = \max(\hat{z}_m, 0)\n\end{cases} \\
\text{trization by introduction} &\begin{cases}\nz_m \leq \hat{z}_m - \underline{h} \quad (1 - a_m) \\
z_m \geq \hat{z}_m\n\end{cases}\n\end{aligned}
$$

o *mth* hidden layer of neural network (NN) with ReLU activation function:

 $\hat{\vec{\zeta}}$  $max(\hat z_m^{\phantom{\dagger}}, \pmb{0})$  $_m = W_m \mathcal{L}_{m-1} + U_m$  $_m$  =  $\text{IIdX}(\mathcal{L}_m)$  $\hat{z}_m = W_m z_{m-1} + b$  $z_m = \max(\hat{z}_m, 0)$  $\left\lceil$  $\left\{ \right.$  $\overline{\mathcal{L}}$ 

*Linearization by introduction binary variables a<sup>m</sup> [1]*:

**omic Dispatch**  
\n
$$
\begin{cases}\n\Delta f_{nadir} = NN_1(\Delta P_e, M, D, R, F, T) \\
\Delta P_{max}^{ibr} = NN_2(\Delta P_e, M, D, R, F, T)\n\end{cases}
$$
\n  
\nidden layer of neural  
\nork (NN) with ReLU  
\nation function:  
\n
$$
\begin{cases}\n\hat{z}_m = W_m z_{m-1} + b_m \\
z_m = \max(\hat{z}_m, 0)\n\end{cases}
$$
\n  
\n
$$
\begin{cases}\nz_m \leq \hat{z}_m - \underline{h} \square (1 - a_m) \\
z_m \geq \hat{z}_m\n\end{cases}
$$
\n  
\n
$$
\begin{cases}\nz_m \leq \bar{h} \square a_m \\
z_m \geq 0\n\end{cases}
$$

![](_page_33_Picture_11.jpeg)

[1] Y. Zhang et al., "Encoding Frequency Constraints in Preventive Unit Commitment Using Deep Learning With Region-of-Interest Active Sampling," *IEEE Trans. Power Syst*., vol. 37, no. 3, pp. 1942–1955, 2022, doi: 10.1109/TPWRS.2021.3110881.

![](_page_34_Figure_1.jpeg)

### ➢ **Deep learning training results**

![](_page_34_Figure_3.jpeg)

- **(a) Training loss** of frequency nadir prediction;
- **(b) Training loss** of IBR peak power prediction;
- **(c) Testing** of frequency nadir prediction;
- **(d) Testing** of IBR peak power prediction.

![](_page_35_Figure_1.jpeg)

➢ **Dynamic Validation Through One-hour Time-domain Simulation**

**ENT** 

![](_page_36_Figure_2.jpeg)

**Dynamics results through full-order time-domain simulation**

# **Microgrid Virtual inertia Scheduling**

### ➢ **Microgrid VIS**

- *Challenge 1*: **Stability guarantee** As device-level control parameters, virtual inertia and damping play a critical role in microgrid stability.
- *Challenge 2*: **Resilient operation** Addressing security constraints, both static and dynamic, during extreme events remains a significant and challenging task.
- ✓ *Model-based? -> Scalability*
- ✓ *Data-driven? -> Reliable Data; Performance Guarantee*
- ✓ *Hybrid Method?*

![](_page_37_Figure_7.jpeg)

**Diagram of islanded microgrid modified from IEEE 123-Bus system**

# **Summary**

- ❑ Although IBRs present **low inertia** characteristics, their **controllability** and **flexibility** allow for the design of an advanced inertia management framework for future low-inertia power grids.
- ❑ **Virtual inertia scheduling (VIS)** is an inertia management concept that targets **security-constrained** and **economy-oriented** inertia scheduling and generation dispatch of microgrids with a large scale of IBRs.
- ❑ The formulation of VIS is quite **flexible** and can be integrated into the conventional economic dispatch framework, but with **customized** decision variables and objective functions, operational conditions, and critical dynamic constraints.

![](_page_38_Picture_4.jpeg)

# **Take-aways**

### ➢ **Core contribution: improve microgrid flexibility and dynamic performance with IBRs**

- ❑ The proposed **P-Q controller** can track the predefined power trajectory with any time constant. It enables the customized response speed of IBRs and thus improved microgrids **flexibility**.
- ❑ The proposed **V-f control framework** can accurately regulation the output of droop-controlled GMF inverters and improve V-f deviation with limited DER capacities. It enables the coordination of P-Q generation, V-f regulation, and demands control, and thus improved microgrids **flexibility**  and **stability**.
- ❑ The proposed **virtual inertia scheduling (VIS)** can effectively management the inertia of IBRpenetrated microgrids, and thus improves microgrid **security**, **stability**, and **economy**.

### ❑ Relevant publications:

- Buxin She, Fangxing Li, Hantao Cui, Jingqiu Zhang, and Rui Bo, "Fusion of Microgrid Control with Model-Free Reinforcement Learning: Review and Vision," *IEEE Transactions on Smart Grid*, vol. 14, no. 4, pp. 3232-3245, July 2023.
- Buxin She, Fangxing Li, Hantao Cui, Hang, Shuai, Oroghene Oboreh-Snapps, Rui Bo, Nattapat Praisuwanna, Jingxin Wang, and Leon M. Tolbert, "Inverter PQ Control with Trajectory Tracking Capability for Microgrids Based on Physics-informed Reinforcement Learning," *IEEE Transactions on Smart Grid*, In-Press, 2023.
- Buxin She, Fangxing Li, Hantao Cui, Jinning Wang, Liang Min, Oroghene Oboreh-Snapps, and Rui Bo, "Decentralized and Coordinated V-f Control for Islanded Microgrids Considering DER Inadequacy and Demand Control," IEEE Transactions on Energy Conversion, vol. 38, no. 3, pp. 1868-1880, Sept. 2023.
- Buxin She, Fangxing Li, Hantao Cui, Jinning Wang, Qiwei Zhang, and Rui Bo, "Virtual Inertia Scheduling for Real-time Economic Dispatch of IBR-penetrated Power Systems," IEEE Transactions on Sustainable Energy, In-Press, 2023.

![](_page_39_Picture_10.jpeg)

### **Acknowledgements**

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![](_page_40_Picture_2.jpeg)

*Other Contributors: Hantao Cui, Jinning Wang, Hang Shuai, Oroghene Oboreh-Snapps, Rui Bo, Nattapat Praisuwanna, Jingxin Wang, Leon M. Tolbert*

![](_page_40_Picture_4.jpeg)

# **Backup Slides**

# **Model-based Analysis (1)**

❑ Derive *k<sup>p</sup>* (*t*) and *k<sup>i</sup>* (*t*) that can ensure the exponential PQ trajectory with specific time constant

![](_page_42_Figure_2.jpeg)

in a general system

RENT

Plug in

![](_page_42_Picture_5.jpeg)

# **Model-based Analysis (2)**<br>  $k_p(t)$  and  $k_l(t)$  that can ensure the exponential PQ trajectory with specific time constant<br>  $= K_p(s) * E(s) + K_i(s) * \frac{E(s)}{s}$ <br>
Exame  $G(s) = \frac{n(s)}{m(s)}$ <br>
Condition 1:  $D[n(s)] = 0$  (D means degree)<br>
(b) =  $L$ **Model-based Analysis (2)**<br>  $E(s) + K_i(s) * \frac{E(s)}{s}$ <br>  $\vdots$ <br>  $\frac{1}{\tau(s+1/\tau)} G(s)$ <br>  $\vdots$ <br>  $\vdots$ <br>  $\tau^* K_i(s) * \frac{1}{s(s+1/\tau)}$ <br>  $\vdots$ <br>  $\vdots$ <br>  $\tau^* K_i(s) * \frac{1}{s(s+1/\tau)}$ <br>  $\vdots$ <br>  $\tau^* K_i(s) * \frac{1}{s(s+1/\tau)}$ <br>  $\vdots$ <br>  $\tau^* K_i(s) * \frac{1}{s(s+1/\tau)}$ <br>  $\$ **Analysis (2)**<br>
hat can ensure the exponential PQ trajectory with specific time constant<br>
(s) e  $\frac{E(s)}{s}$ <br>  $\frac{1}{\pi(s)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ <br>  $\frac{1}{\pi(s+1/\tau)}$ **Model-based Analysis (2)**<br>
and  $k(t)$  that can ensure the exponential PQ trajectory with specific time constant<br>
(x) + E(s) + K<sub>z</sub>(s) + E(s) = E **Model-based Analysis (2)**<br>
that can ensure the exponential PQ trajectory with specific time constant<br>  $K_s(s) * \frac{E(s)}{s}$ <br>  $\overbrace{S(s)}^{(s)}$ <br>  $\overbrace{S(s+1/\tau)}^{(1-\tau)}$ <br>  $\begin{cases}\n\text{Conclusion:} & \text{for } s = \frac{n(s)}{m(s)} \\
\hline\n\end{cases}$ <br>  $\begin{cases}\n\text{Equation 1:} & D[n$ **Model-based Analysis (2)**

❑ Derive *k<sup>p</sup>* (*t*) and *k<sup>i</sup>* (*t*) that can ensure the exponential PQ trajectory with specific time constant

➢ Step 3:

$$
\frac{Y(s)}{G(s)} = K_p(s) * E(s) + K_i(s) * \frac{E(s)}{s}
$$

• For the left side:

$$
\mathcal{L}^{-1}\left[\frac{Y(s)}{G(s)}\right] = \mathcal{L}^{-1}\left[\frac{1}{\tau s(s+1/\tau)}\cdot G(s)\right]
$$

• For the right side:

Model-based Analysis (2)					
\n <p>erive <math display="block">k_p(t)</math> and <math>k_i(t)</math> that can ensure the exponential PQ trajectory with specific time constant</p> \n					
\n <p>ep 3:</p> \n $\frac{Y(s)}{G(s)} = K_p(s) * E(s) + K_i(s) * \frac{E(s)}{s}$ \n	\n <p>Conclusion:</p> \n <p>Assume <math>G(s) = \frac{n(s)}{m(s)}</math></p> \n				
\n <p>or the left side:</p> \n $L^{-1}[K_p(s) * \frac{1}{s+1/\tau} + K_i(s) * \frac{1}{s(s+1/\tau)} \cdot G(s)]$ \n	\n <p>of the right side:</p> \n $L^{-1}[K_p(s) * \frac{1}{s+1/\tau} + K_i(s) * \frac{1}{s(s+1/\tau)}]$ \n	\n <p>of the right side:</p> \n $L^{-1}[K_p(s) * \frac{1}{s+1/\tau} + K_i(s) * \frac{1}{s(s+1/\tau)}]$ \n	\n <p>of the right side is</p> \n $L^{-1}[K_p(s) * \frac{1}{s+1/\tau} + K_i(s) * \frac{1}{s(s+1/\tau)}]$ \n	\n <p>of the right side is</p> \n $L^{-1}[K_p(s) + K_p(s) * \frac{1}{s(s+1/\tau)}]$ \n	\n <p>of the right side is</p> \n $L^{-1}[K_p(s)] = O(Dm(s) - D[m(s)] \leq 2$ \n
\n <p>from transfer function <math>G(s)</math></p> \n <p>from this equation in time domain.</p> \n	\n <p>Condition 3:</p> \n $D[n(s)] - D[m(s)] > 2$ \n <p>Proof of the right side is</p> \n $k_i(t) = \frac{L^{-1}[\frac{L(s)}{s \cdot m(s)}]}{t \cdot m(s)}$ \n				
\n <p>From this equation in time domain.</p> \n	\n <p>Condition 4:</p> \n $L^{-1}[K_p(s) * \frac{1}{s+1/\tau} + K_i(s) * \frac{1}{s(s$				

System transfer function *G*(s) determines whether 'left side = right side' has a solution in time domain.

### *Conclusion:*

Assume 
$$
G(s) = \frac{n(s)}{m(s)}
$$

**Analysis (2)**<br>
nential PQ trajectory with s<br> **Conclusion:**<br>
Assume  $G(s) = \frac{n(s)}{m(s)}$ <br>  $\checkmark$  Condition 1:  $D[n(s)] = 0$  (Dm<br>  $\begin{cases} k_p(t) = l_1 + l_2 \\ k_i(t) = \frac{l_2}{\tau} \end{cases}$  $\begin{array}{ll}\n\textbf{(s)} \\
\textbf{(s)} \\
\text$ **n y sis (2)**<br>
PQ trajectory with sp<br>
<u>sion:</u><br>  $G(s) = \frac{n(s)}{m(s)}$ <br>
ion 1:  $D[n(s)] = 0$  (D me<br>  $\begin{cases} k_p(t) = l_1 + l_2 \\ k_i(t) = \frac{l_2}{\tau} \end{cases}$ **is (2)**<br>
ajectory with sp<br>  $\frac{n(s)}{m(s)}$ <br>  $D[n(s)] = 0$  (D me<br>  $\begin{cases} k_p(t) = l_1 + l_2 \\ k_i(t) = \frac{l_2}{\tau} \end{cases}$  $\checkmark$  Condition 1:  $D[n(s)] = 0$  (D means degree) **S (2)**<br> *D* ajectory with specific time<br>  $\frac{n(s)}{n(s)}$ <br>  $D[n(s)] = 0$  (D means degree)<br>  $\begin{cases} k_p(t) = l_1 + l_2 \\ k_i(t) = \frac{l_2}{l_1} \end{cases}$ 

$$
\begin{cases}\nk_p(t) = l_1 + l \\
k_i(t) = \frac{l_2}{\tau}\n\end{cases}
$$

 $\checkmark$  Condition 2:  $D[n(s)] \neq 0, D[n(s)] - D[m(s)] \leq 2$ 

**Analysis (2)**  
\nmental PQ trajectory with specific time constant  
\n**Conclusion:**  
\nAssume 
$$
G(s) = \frac{n(s)}{m(s)}
$$
  
\n $\checkmark$  Condition 1:  $D[n(s)] = 0$  (*D* means degree)  
\n
$$
\begin{cases}\nk_p(t) = l_1 + l_2 \\
k_i(t) = \frac{l_2}{\tau}\n\end{cases}
$$
\n $\checkmark$  Condition 2:  $D[n(s)] \neq 0, D[n(s)] - D[m(s)] \leq 2$   
\n
$$
\begin{cases}\nk_p(t) = l_1 + \mathcal{L}^{-1}[\frac{l_2(s)}{s \cdot n(s)}] \\
k_i(t) = \frac{\mathcal{L}^{-1}[\frac{l_2(s)}{s \cdot n(s)}]}{\tau}\n\end{cases}
$$
\n $\checkmark$  Condition 3:  $D[n(s)] - D[m(s)] > 2$   
\n $k_p(t)$  and  $k_i(t)$  don't exist

# **Data-driven Implementation: DRL**

![](_page_44_Figure_1.jpeg)

### **Reinforcement learning :**

❑ RL is a basic machine paradigm formulated as a Markov Decision Processes.

### **Deep reinforcement learning:**

❑ Use **deep neural network** to map: State, action  $\rightarrow$  value (Q-value); State  $\longrightarrow$  action

### **Training Target:**

❑ *a well-trained RL agent chooses optimal actions for maximum accumulated reward (best performance)*

![](_page_44_Picture_8.jpeg)

# **Comparison(1)**

![](_page_45_Figure_1.jpeg)

➢ **Scenario 1-1**: Scheduling *Pref* change ➢ **Scenario 1-2**: Scheduling *Pref* and *Qref* change

![](_page_45_Figure_3.jpeg)

Where  $\Delta P = P_{inv} - P_{tri}$  is real-time trajectory tracking error.

# **Comparison(2)**

![](_page_46_Figure_1.jpeg)

![](_page_46_Figure_2.jpeg)

➢ **Scenario 3**: Grounded fault

![](_page_46_Figure_4.jpeg)

Where  $\Delta P = P_{inv} - P_{tri}$  is real-time trajectory tracking error.

# **Summary**

- ❑ The **system transfer functions** are categorized into three conditions, determining whether there exists a time-varying-gain adaptive PI controller that can track an exponentially traceable curve.
	- o In *Condition 1*, fixed-gains work;
	- o in *Condition 2*, time-varying gains are required;
	- o in *Condition 3*, no adaptive PI controller works.
- ❑ The microgrid inverter-based PQ control system meets *Condition 2*. After implementing the proposed adaptive PI controller, the active and reactive power output of inverters can **track a predefined exponential trajectory**.
- ❑ The proposed controller outperforms the conventional fixed-gain and adaptive PI controllers. **Without manual re-tuning**, it can accurately track the predefined trajectory with any assigned time constant.
- ❑ The **model-based analysis** provides guidelines for deep RL training, which relieves the training pressure and saves training time. In turn, the implementation of **physics-informed deep RL**  solves the problem of unavailability and uncertainty in the model-based method.

![](_page_47_Picture_8.jpeg)